

Fig. 3.12: Amplitude and phase response of a Titan element in a $\frac{1}{2}$ " package (from [3]).

The frequency and phase response of a Microflow can be represented in terms of an electronic model of the device, with the output of an “ideal” Microflow {having flat frequency and phase response} subsequently altered by three passive RC -type networks to emulate the low frequency and high frequency behavior of the device, as shown in the figure below:

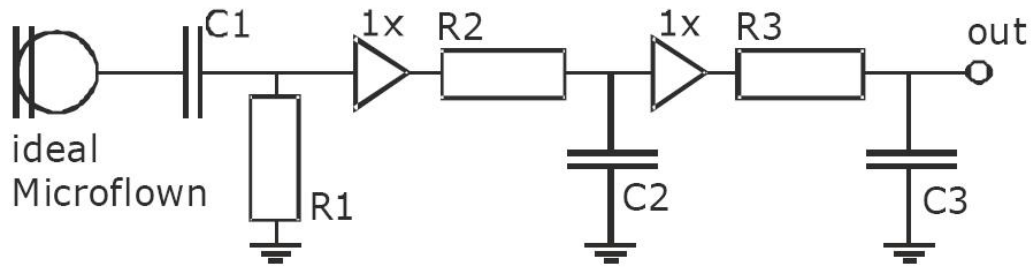


Fig. 3.6: Electrical model of the frequency dependent behaviour of a Microflow.

Using this electrical model to represent an actual Microflow, the frequency and phase response of the device are approximately given by:

$$V_{out}(f) \approx V_{out}(250\text{Hz}) \cdot \frac{1}{\sqrt{1+(f_{blay}/f)^2}} \cdot \frac{1}{\sqrt{1+(f/f_{difn})^2}} \cdot \frac{1}{\sqrt{1+(f/f_{hrcp})^2}}$$

and:

$$\varphi(f) \approx \tan^{-1}(f_{blay}/f) - \tan^{-1}(f/f_{difn}) - \tan^{-1}(f/f_{hrcp})$$

A signal conditioner is used on the Microflow output signal to correct (*i.e.* undo/invert) the frequency and phase response such that both are flat at the output of the signal conditioner.