The (complex) frequency response of the simple op-amp integrator preamplifier circuit is:

$$
\tilde{H}_{\text{oai}}(\omega) = \left(R_{\text{fb}}/R_{\text{I}}\right) \cdot \frac{1}{1 + i\omega R_{\text{fb}}C} = \left(R_{\text{fb}}/R_{\text{I}}\right) \cdot \frac{1}{1 + i\omega \tau_{\text{fb}}} \quad \{\text{using: } \tau_{\text{fb}} \equiv R_{\text{fb}}C \text{ (sec)}\}
$$

At low frequencies, such that  $\omega \ll 1/R_p C = 1/\tau_p$ :  $\tilde{H}_{oai} (\omega \ll 1/R_p C) = (R_p/R_1)$  is a purely *real* quantity – *i.e.* the output of the op-amp integrator is *in-phase* with the input. At high frequencies, such that  $\omega \gg 1/R_{fb}C = 1/\tau_{fb}$  then:  $\tilde{H}_{oai}(\omega \gg 1/R_{fb}C) \approx (R_{fb}/R_1) \cdot \frac{1}{\tau_{bf}R_0} = -i \frac{(R_{fb}/R_1)}{R_0R_0}$  $f_b$  *w* $\mathbf{w}$  $\mathbf{h}$  $R_{_{fb}}/R$  $H_{\rho q i}(\omega \gg 1/R_{\phi}C) \simeq (R_{\phi}/R_{\phi}) \cdot \frac{1}{\sqrt{R_{\phi}C}} = -i$  $\omega \gg 1/R_{fb}C = (R_{fb}/R_1) \cdot \frac{1}{i\omega R_{fb}C} = -i \frac{1}{\omega R_{fb}C}$  $\tilde{H}_{\text{oai}}\left(\omega \gg 1/R_{\text{fb}}C\right) \approx \left(R_{\text{fb}}/R_1\right) \cdot \frac{1}{i\omega R_{\text{B}}C} = -i\frac{(R_{\text{fb}}/R_1)}{\omega R_{\text{B}}C}$  and thus

we see that the high-frequency output response of the op-amp integrator is proportional to  $1/\omega$ and is -90<sup>°</sup> *out-of-phase* with the input signal. The frequency and phase response of the simple op-amp integrator circuit (alone) is shown in the figure below.



Note that the phase response of this op-amp integrator circuit is  $\sim$  constant in the frequency range  $\sim$  50  $Hz < f < \sim$  4  $KHz$ , which is of primary interest for most musical instruments.

 This simple op-amp integrator circuit is used in conjunction with a modified version of the Knowles Electronics EK-23132 subminiature electret condenser microphone (with back plate removed and replaced with a very fine-mesh copper screen {electrically connected to mic case using conductive epoxy paint for RFI/EMI suppression}) for a 1-D particle velocity microphone. Note that well above the  $-3$  dB low-frequency pole of the op-amp integrator circuit (*i.e.*  $\omega \gg 1/R<sub>f</sub>C$  ) but still well below  $\omega \ll c/d$ , the combined response of the differential pressure microphone + op-amp integrator circuit is constant, independent of (angular) frequency  $\omega$ .

$$
\widetilde{H}_{u-mic}(\omega,\Theta)\Big|_{1/R_fC\ll \omega\ll c/d} = \widetilde{H}_{diff-mic}(\omega,\Theta)\cdot \widetilde{H}_{oai}(\omega)\Big|_{1/R_fC\ll \omega\ll c/d} \simeq \left(\frac{d}{c}\right)\left(\frac{R_{fb}/R_1}{R_{fb}C}\right)\cos\Theta
$$

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