Likewise, the real and imaginary parts of the complex radial acoustic energy flow velocity are:

$$c_{a_{r}}^{r}\left(r,\omega\right) = \operatorname{Re}\left\{\tilde{c}_{a_{r}}\left(r,\omega\right)\right\} = c\frac{1}{\left[1 + \left(1/kr\right)^{2}\right]} \quad \text{and:} \quad c_{a_{r}}^{i}\left(r,\omega\right) = \operatorname{Im}\left\{\tilde{c}_{a_{r}}\left(r,\omega\right)\right\} = c\frac{1/kr}{\left[1 + \left(1/kr\right)^{2}\right]}$$

The phase of the complex radial <u>specific</u> acoustic impedance and complex radial acoustic energy flow velocity is:

$$\varphi_{z_a} = \varphi_{c_a} = \Delta \varphi_{p-u} = \varphi_p - \varphi_u = \tan^{-1}(1/kr)$$

- (a) In the "near" zone: $kr \ll 1$, the complex radial <u>specific</u> acoustic impedance and the complex radial energy flow velocity are both largely <u>imaginary</u> (i.e. <u>reactive</u>): $\tilde{z}_{a_r}(r)/z_o = \tilde{c}_{a_r}(r)/c = [1+i/kr]/[1+(1/kr)^2] \sim i \cdot kr$, increasing \sim linearly with r, with fractional magnitude $|\tilde{z}_{a_r}(r)|/z_o = |\tilde{c}_{a_r}(r)|/c = 1/\sqrt{1+(1/kr)^2} \sim kr \ll 1$ and phase $\varphi_{z_a} = \varphi_{c_a} = \varphi_p \varphi_u = \tan^{-1}(1/kr) \sim \tan^{-1}(\infty) \sim 90^\circ$. Again, the complex sound field $\tilde{S}(\vec{r},t)$ in this region is <u>inertia</u>-like (i.e. <u>mass</u>-like), because $z_{a_r}^i(r) = \operatorname{Im}\{\tilde{z}_{a_r}(r)\} > 0$ for $kr \ll 1$.
- (b) In the "intermediate zone: $kr \sim 1$, the complex radial specific acoustic impedance and the complex radial energy flow are both \sim an equal mix of active (i.e. real) and reactive (i.e. imaginary) components: $\tilde{z}_{a_r}(r)/z_o = \tilde{c}_{a_r}(r)/c = [1+i/kr]/[1+(1/kr)^2] \sim (1+i)/2$, with fractional magnitude $|\tilde{z}_{a_r}(r)|/z_o = |\tilde{c}_{a_r}(r)|/c = 1/\sqrt{1+(1/kr)^2} \sim 1/\sqrt{2}$ and phase $\varphi_{z_o} = \varphi_{c_o} = \varphi_p \varphi_u = \tan^{-1}(1/kr) \sim \tan^{-1}(1) \sim 45^\circ$.
- (c) In the "far" (or radiation) zone: $kr \gg 1$, the complex radial <u>specific</u> acoustic impedance and the complex radial energy flow velocity are largely <u>real</u> (i.e. <u>active</u>): $\tilde{z}_{a_r}(r)/z_o = \tilde{c}_{a_r}(r)/c = 1/[1+(1/kr)^2] \sim 1 \text{ with magnitude}$ $\left|\tilde{z}_{a_r}(r)\right|/z_o = \left|\tilde{c}_{a_r}(r)\right|/c = 1/\sqrt{1+(1/kr)^2} \sim 1 \text{ and phase}$ $\varphi_{z_o} = \varphi_{c_o} = \varphi_p \varphi_u = \tan^{-1}(1/kr) \sim \tan^{-1}(0) \sim 0^\circ.$

The <u>frequency domain</u> complex radial acoustic intensity associated with the point acoustic monopole also points outward in the radial (\hat{r}) direction; it and its magnitude are:

$$\tilde{I}_{a_{r}}\left(r,\omega\right) \equiv \frac{1}{2}\,\tilde{p}\left(r,\omega\right) \cdot \tilde{u}_{r}^{*}\left(r,\omega\right) = \frac{1}{2}\,\frac{1}{z_{o}}\,\frac{B_{o}^{2}}{r^{2}}\left[1 + \frac{i}{kr}\right] \quad \text{and:} \quad \left|\tilde{I}_{a_{r}}\left(r,\omega\right)\right| = \frac{1}{2}\,\frac{1}{z_{o}}\,\frac{B_{o}^{2}}{r^{2}}\sqrt{1 + \left(1/kr\right)^{2}}$$

The real and imaginary parts of the *frequency domain* radial complex acoustic intensity are:

$$I_{a_{r}}^{r}(r,\omega) = \operatorname{Re}\left\{\tilde{I}_{a_{r}}(r,\omega)\right\} = \frac{1}{2} \frac{1}{z_{o}} \frac{B_{o}^{2}}{r^{2}} \quad \text{and:} \quad I_{a_{r}}^{i}(r,\omega) = \operatorname{Im}\left\{\tilde{I}_{a_{r}}(r,\omega)\right\} = \frac{1}{2} \frac{1}{z_{o}} \frac{B_{o}^{2}}{r^{2}} \frac{1}{kr}$$