

Example # 1: 1-D Plane Monochromatic Traveling Wave Propagating in “Free Air”:

In “*free air*”, the *instantaneous time-domain* pressure at a space-time point (x, t) associated with a 1-D plane monochromatic traveling wave propagating *e.g.* in the $+x$ -direction is a *purely real* quantity: $p(x, t) = p_o \cos(\omega t - kx)$.

The 1-D *instantaneous time-domain* longitudinal particle velocity (*i.e.* in the $+x$ -/propagation direction) at the space-time point (x, t) associated with a 1-D plane monochromatic traveling wave is obtained via the {linearized} 1-D Euler equation for inviscid fluid flow:

$$\frac{\partial u^{\parallel}(x, t)}{\partial t} = -\frac{1}{\rho_o} \frac{\partial p(x, t)}{\partial x} = -\frac{p_o}{\rho_o} \frac{\partial \cos(\omega t - kx)}{\partial x} = -\frac{kp_o}{\rho_o} \sin(\omega t - kx)$$

Then:

$$u^{\parallel}(x, t) = -\frac{kp_o}{\rho_o} \int \sin(\omega t - kx) dt = +\frac{kp_o}{\omega \rho_o} \cos(\omega t - kx) = \frac{p_o}{\rho_o c} \cos(\omega t - kx) = u_o^{\parallel} \cos(\omega t - kx)$$

where we have used the relation $c = \omega/k = 343 \text{ m/s} =$ speed of sound in {bone-dry} air @ NTP (obtained from the 1-D wave equation(s) for p or u^{\parallel}). Note also that: $u_o^{\parallel} = p_o / \rho_o c = p_o / z_o$.

Since $p(x, t) = p_o \cos(\omega t - kx)$ and $u^{\parallel}(x, t) = (p_o / \rho_o c) \cos(\omega t - kx) = u_o^{\parallel} \cos(\omega t - kx)$, we see that the *instantaneous time-domain* pressure and longitudinal particle velocity are *in-phase* with each other for a 1-D monochromatic plane wave propagating in “*free air*”. This in turn implies that for *harmonic* (*i.e.* single-frequency) {aka monochromatic} plane waves, the longitudinal *specific* acoustic impedance, *specific* admittance and intensity will thus also be *purely real* quantities for a 1-D monochromatic plane wave propagating in “*free air*”

We then “complexify” the above *instantaneous time-domain* pressure and longitudinal particle velocity expressions to obtain their complex *time-domain* representations:

$\tilde{p}(x, t) = p_o e^{i(\omega t - kx)}$ and $\tilde{u}^{\parallel}(x, t) = u_o^{\parallel} e^{i(\omega t - kx)}$. The longitudinal *specific* acoustic impedance associated with a 1-D monochromatic plane wave propagating *e.g.* in the $+x$ -direction in “*free air*” is then easily seen to {also} be a *purely real* quantity:

$$\tilde{z}_a^{\parallel}(x) = \frac{\tilde{p}(x, t)}{\tilde{u}^{\parallel}(x, t)} = \frac{p_o e^{i(\omega t - kx)}}{u_o^{\parallel} e^{i(\omega t - kx)}} = \frac{p_o}{u_o^{\parallel}} = \frac{p_o}{p_o / \rho_o c} = \rho_o c \equiv z_o \quad (\Omega_a)$$

Since {here} $\tilde{z}_a^{\parallel}(x) = \rho_o \tilde{c}_a^{\parallel}(x)$, we see that the longitudinal velocity of energy flow $\tilde{c}_a^{\parallel}(x) = c$ for a 1-D monochromatic plane wave propagating *e.g.* in the $+x$ -direction in “*free air*”.

Note that this acoustic sound field example is the electrical analog of a simple AC circuit, *e.g.* driven at constant voltage by a sine-wave generator with a *purely real instantaneous* AC voltage $V(t) = V_o \cos \omega t$ imposed across an *ideal* resistor of resistance R (Ω) (hence *purely real* impedance $\tilde{Z} = R + i0$ (Ω_e)) resulting in a *purely real instantaneous* AC current $I(t) = I_o \cos \omega t$ flowing through it.