

Next, we explain why $\tilde{z}_a(\vec{r}, \omega)$ and $\tilde{y}_a(\vec{r}, \omega) = 1/\tilde{z}_a(\vec{r}, \omega)$ are called complex \Rightarrow **specific** \Leftarrow acoustic impedance and admittance, respectively. As mentioned above, $\tilde{z}_a(\vec{r}, \omega)$ and $\tilde{y}_a(\vec{r}, \omega) = 1/\tilde{z}_a(\vec{r}, \omega)$ are immittances **specifically** associated with the propagation medium. And, in order to avoid confusion, there {already} exists two **other** acoustic immittance quantities, known as the complex 3-D vector acoustic impedance $\tilde{Z}_a(\vec{r}, \omega)$ and the complex 3-D vector acoustic admittance $\tilde{Y}_a(\vec{r}, \omega) = 1/\tilde{Z}_a(\vec{r}, \omega)$, which are associated with the acoustics of sound waves propagating inside **ducts** (*i.e.* pipes) with cross-sectional area S_\perp as defined below:

Complex 3-D Acoustic Immittances (for Harmonic Sound Fields):

Complex 3-D Acoustic Impedance:

$$\tilde{Z}_a(\vec{r}, \omega) \equiv \frac{\tilde{p}(\vec{r}, \omega)}{\tilde{u}(\vec{r}, \omega) S_\perp} = \frac{1}{\tilde{Y}_a(\vec{r}, \omega)} \left(\begin{array}{l} Pa\cdot s/m^3 \\ = N\cdot s/m^5 = Rayl/m^2 \end{array} \right)$$

Complex 3-D Acoustic Admittance:

$$\tilde{Y}_a(\vec{r}, \omega) \equiv \frac{\tilde{u}(\vec{r}, \omega) S_\perp}{\tilde{p}(\vec{r}, \omega)} = \frac{1}{\tilde{Z}_a(\vec{r}, \omega)} \left(\begin{array}{l} m/Pa\cdot s \\ = m^3/N\cdot s = Rayl^{-1}\cdot m^2 \end{array} \right)$$

Note that the quantity $\tilde{U}(\vec{r}, \omega) \equiv \tilde{u}(\vec{r}, \omega) S_\perp$ ($m/s \cdot m^2 = m^3/s$) is known as the **volume velocity**, because of its dimensions (m^3/s).

Inside a duct of cross sectional area S_\perp , the complex 3-D vector **specific** acoustic immittances $\tilde{z}_a(\vec{r}, \omega)$ and $\tilde{y}_a(\vec{r}, \omega) = 1/\tilde{z}_a(\vec{r}, \omega)$ are thus related to the complex 3-D vector immittances $\tilde{Z}_a(\vec{r}, \omega)$ and $\tilde{Y}_a(\vec{r}, \omega) = 1/\tilde{Z}_a(\vec{r}, \omega)$ by the relations:

$$\tilde{z}_a(\vec{r}, \omega) = \tilde{Z}_a(\vec{r}, \omega) S_\perp \quad \text{and} \quad \tilde{y}_a(\vec{r}, \omega) = \tilde{Y}_a(\vec{r}, \omega) / S_\perp$$

or:

$$\tilde{Z}_a(\vec{r}, \omega) = \tilde{z}_a(\vec{r}, \omega) / S_\perp \quad \text{and} \quad \tilde{Y}_a(\vec{r}, \omega) = \tilde{y}_a(\vec{r}, \omega) S_\perp$$

From the above relations, since the complex 3-D vector **specific** acoustic immittances $\tilde{z}_a(\vec{r}, \omega)$ and $\tilde{y}_a(\vec{r}, \omega) = 1/\tilde{z}_a(\vec{r}, \omega)$ are manifestly **frequency domain** quantities, we see that the complex 3-D vector acoustic immittances $\tilde{Z}_a(\vec{r}, \omega)$ and $\tilde{Y}_a(\vec{r}, \omega) = 1/\tilde{Z}_a(\vec{r}, \omega)$ are also manifestly **frequency domain** quantities.